



Plaster and Façade Systems

P914\_TB.de
Technical Brochure 2024-05

# **MP 75 Fire**Fire Protection Gypsum Plaster

Planing Guide



■ New formulation with fibre-reinforced plaster



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MP 75 Fire
Fire Protection Gypsum Plaster



#### **Product description**

MP 75 Fire has been developed specially for fire protection of buildings in interiors. Its task is to protect the load bearing coated construction elements in the event of a fire so that their function is maintained until the fire has been extinguished or building evacuated.

MP 75 Fire consists of gypsum as a binder in combination with a special mix of lightweight aggregates, additives and fibres to ensure good machine application. MP 75 Fire has been granted the European Technical Approval ETA-21/0727.

#### Field of application

- Concrete ceilings and walls acc. to DIN EN 1992-1-2
- Concrete beams and supports acc. to DIN EN 1992-1-2
- Steel columns and beams acc. to DIN EN 1993-1-2
- Special constructions acc. to DIN 4102-4

#### Properties and added value

- Easy machine application
- Gypsum based
- Fibre reinforced
- Colour white

#### **Technical data**

Description	Standard	Unit	MP 75 Fire
Reaction to fire	EN 13501-1	-	A1
Compressive strength	EN 13279-2	N/mm <sup>2</sup>	≥2.3
Tensile bond strength     On concrete     On steel	EN 1015-2	N/mm <sup>2</sup> N/mm <sup>2</sup>	≥ 0.2 ≥ 0.15
Water vapour diffusion resistance	EN 12086	-	7
pH value	-	-	12 – 13
Initial setting time	-	min	approx. 90 – 170
Final setting time	-	min	approx. 180 – 300
Bulk density	-	kg/m <sup>3</sup>	500 – 600
Dry density	EN 1015-10	kg/m <sup>3</sup>	approx. 750
Bending tensile strength	EN 13279-2	N/mm <sup>2</sup>	1.0
Thermal conductivity $\lambda_{10,dry}$	EN 1745	W/m·K	0.20
Wet mortar weight	-	kg/mm/m <sup>2</sup>	approx. 1.3
Dry plaster weight	-	kg/mm/m <sup>2</sup>	approx. 0.8

The stated technical data were evaluated acc. to the respective test standards. Deviations under site conditions are possible.

#### **Material requirement and efficiency**

Application	Consumption approx.	Yield approx.	
	kg/m <sup>2</sup>	m <sup>2</sup> /bag	m²/t
10 mm application thickness	6.2	3.2	161.0

All stated figures are approximate values and may deviate depending on the substrate conditions. The exact consumption can only be determined on the individual object.

#### Notes on fire resistance

The application options and the fire protection properties of the MP 75 Fire stated here are based on the data of the European Technical Approval ETA -21/0727 and the test reports on which it is based. All specifications marked with offer the user additional application options, which are not directly included in the European Certificate of Usability, but which have been technically assessed on the basis of the Experts Opinions BB-23-325-1 & -2 by IBB Hauswaldt.

The basis for the Experts Opinions BB-23-325-1 & -2 are, in addition to the DIN 4102-4 (Fire behaviour of building materials and building components) and the DIN EN 133813 /-4 (Test methods for determining the contribution to the fire resistance of structural members), the test reports of the MFPA Leipzig on which the ETA-21/0727 is based.

Knauf wishes to point out that before the fire protection enhancement with MP 75 Fire, the construction and implementation including all those in the planning aid marked with plus should in every case be coordinated and

authorised in advance in consultation between the persons responsible for fire resistance and/or the relevant authorities. Technical Brochure P914\_TB provides an overview of all areas of application classified as feasible from a fire resistance perspective. The application thicknesses specified here are compliant with ETA-21/0727 or were calculated in accordance with the specifications of the DIN EN 1992-1-2 (Eurocode 2: Design of concrete structures - Part 1 – 2: General rules – Structural fire design). All application thicknesses are valid exclusively when the stated specifications are complied with in detail.

The layer thicknesses specified are minimum thicknesses that must be observed. It is not permissible to apply a second layer after the fire protection plaster has hardened. For this reason, we recommend application of a layer thickness that is always 10 to 20 % more than the minimum to avoid the risk of layer thicknesses that are too thin.



**Concrete constructions** 

Fire resistance coating of concrete components





#### Field of application

#### 1-sided exposed concrete walls and slabs

- For a concrete density in a range of 1955 kg/m³ to 2725 kg/m³.
- Concrete strength class at least C30/37 up to and including C50/60.
- Fire resistance classes 30 to 180 minutes



- Concrete density of 800 kg/m³ to 1954 kg/m³
- Concrete classes < C30/37

The rating of the application thickness of MP 75 Fire required for fire resistance purposes on concrete components is in accordance with the tables on the following pages and depends on

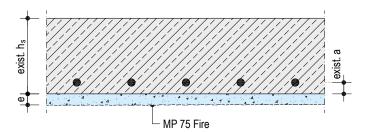
- Constructional component and loading
- Required fire resistance class according to building authority requirements
- Demands on the concrete thickness acc. to DIN EN 1992-1-2, section 5 for the necessary fire resistance class
- Existing concrete thickness
- Equivalent thickness of concrete of the ETA-21/0727

#### **Procedure**

- 1. Observe the fields of application.
- 2. Determine the required thicknesses of concrete (req. a and req.  $h_{\rm s}$ ) acc to DIN EN 1992-1-2, section 5.
- Determine the existing concrete thickness (exist. a and exist. h<sub>s</sub>) and derive the decisive (maximum) missing concrete thickness.
- Read off the minimum plaster layer thickness e for MP 75 Fire in accordance with the missing concrete thickness from the tables on the following pages.

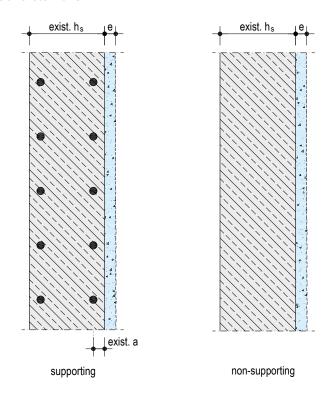
For rating examples see "Rating example" on page 11.

#### **Concrete covers**



exist. a = existing axial spacing
exist. h<sub>s</sub> = existing slab thickness
e = thickness MP 75 Fire

#### **Concrete walls**



exist. a = existing axial spacing with supporting walls

exist. h<sub>s</sub> = existing wall thickness e = thickness MP 75 Fire



# Technical fire resistance assessed acc. to Experts Opinion BB-23-325-1 & -2

■ Prior consultation is recommended acc. to note on page 5

## **Concrete constructions**



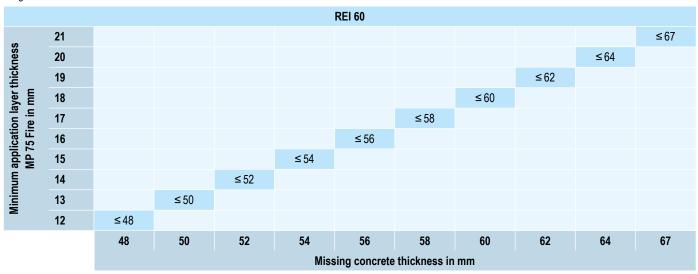


## Minimum application layer thickness e

#### In dependence on the fire resistance class and missing concrete thickness

Diagram 1

						REI 30					
	21					112100					≤50
SS										z 10	<u> </u>
kne	20									≤49	
Ē_	19								≤ 47		
ağe m	18							≤46			
on Re in	17						≤45				
icati '5 Fi	16					≤43					
application layer MP 75 Fire in mm	15				≤42						
Minimum application layer thickness MP 75 Fire in mm	14			≤40							
Ē	13		≤39								
2	12	≤38									
		38	39	40	42	43	45	46	47	49	50
					Miss	sing concrete	thickness in	mm			

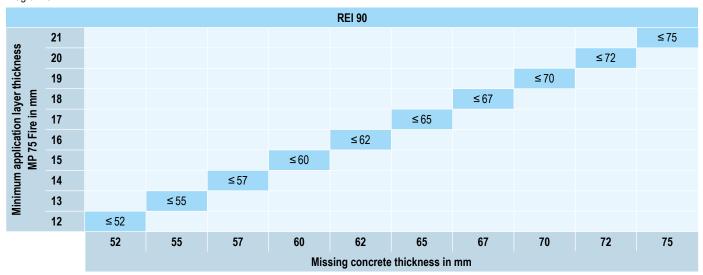


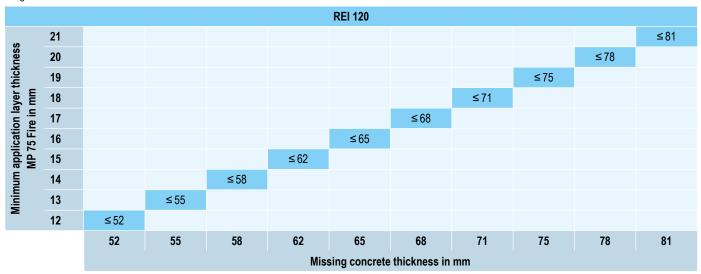


## Minimum application layer thickness e (continuation)

#### In dependence on the fire resistance class and missing concrete thickness

Diagram 3





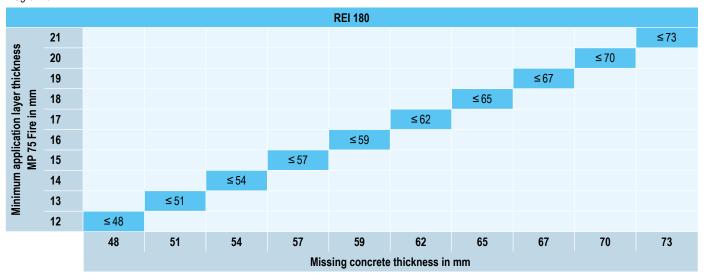
## **Concrete constructions**





## Minimum application layer thickness e (continuation)

In dependence on the fire resistance class and missing concrete thickness





#### Rating example

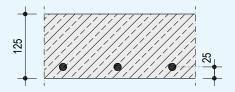
Structurally determined supported, twin-axis stressed reinforced concrete ceiling with side ratio 1.5 <  $I_y/I_x \le 2.0$  and supported on all 4 edges acc. to DIN EN 1992-1-2, section 5, table 5.8, columns 2 and 5

Required fire resistance class: REI 180

Concrete density: 2100 kg/m³

Concrete strength class C25/30

Slab dimensions:



Step 1

#### Checking of the prerequisites acc. to ETA-21/0727

- Concrete density = 2100 kg/m³ ranges between 1955 kg/m³ to 2725 kg/m³
- Concrete strength class C25/30 is at least C25/30

#### Step 2

Requirements in the minimum axial spacing acc. to DIN EN 1992-1-2, section 5, table 5.8, columns 2 and 5  $\,$ 

■ req. a = 40 mm

#### Step 3

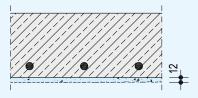
#### Deriving the missing concrete thickness

■ req.  $h_s$  - exist.  $h_s$  = 150 mm - 125 mm = 25 mm ■ req. a - exist. a = 40 mm - 25 mm = 15 mm Decisive missing concrete thickness = 25 mm

#### Step 4

#### Deriving the min. layer thickness for MP 75 Fire

■ Diagram 5 (see page 10): **e = 12 mm** 



#### Concrete constructions

#### Columns and beams



#### Field of application

#### 3-sided or 4-sided exposed concrete beams and columns

- For a concrete density in a range of 1955 kg/m³ to 2725 kg/m³
- Column / beam width of at least 150 mm
- Beam height of at least 450 mm
   Lower heights are possible if the cross-sectional area is not reduced.
- Concrete strength class C30/37 up to and including C50/60.
- Fire resistance classes 30 to 180 minutes



- 1-sided or 2-sided exposed concrete beams and columns
- Concrete density of 800 to 1954 kg/m<sup>3</sup>
- Concrete classes < C30/37
- Column / beam width of 80 149 mm
- Applications acc. to DIN 4102-4



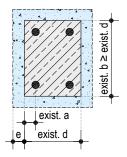
The rating of the application thickness of MP 75 Fire required for fire resistance purposes on concrete components is in accordance with the tables on the following pages and depends on

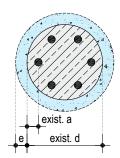
- Constructional component and loading
- Required fire resistance class according to building authority requirements
- Demands on the concrete thickness acc. to DIN EN 1992-1-2, section 5 for the necessary fire resistance class
- Existing concrete thickness
- Equivalent thickness of concrete of the ETA-21/0727

#### **Procedure**

- 1. Observe the fields of application.
- 2. Determine the required concrete thickness (req. a and req. b or req. d) acc to DIN EN 1992-1-2, section 5.
- 3. Determine the existing concrete thickness (exist. a and exist. b or exist. d) and derive the decisive (maximum) missing concrete thickness.
- Read off the minimum plaster layer thickness e for MP 75 Fire in accordance with the missing concrete thickness from the tables on the following pages.

For rating examples see page 15.





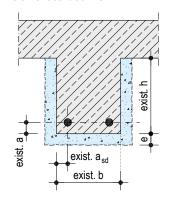
exist. a = existing axial spacing

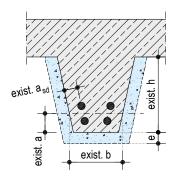
exist. b = larger existing column width

exist. d = smaller existing column width or diameter

e = thickness MP 75 Fire

#### **Concrete beams**





exist. a = existing axial spacing

exist. a<sub>sd</sub> = existing lateral axial spacing

exist. b = existing beam width in the height of the

center of gravity of the tensile area reinforcement

exist. h = existing beam height e = thickness MP 75 Fire



Technical fire resistance assessed acc. to Experts Opinion BB-23-325-1 & -2

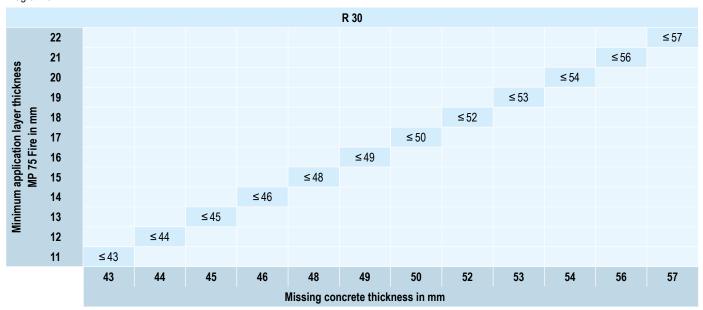
■ Prior consultation is recommended acc. to note on page 5

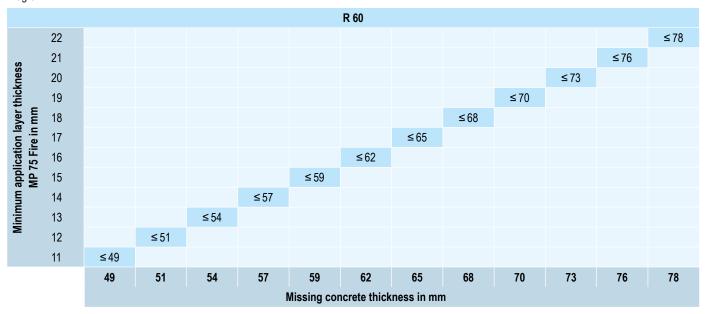


#### Minimum application layer thickness e

#### In dependence on the fire resistance class and missing concrete thickness

Diagram 6





## **Concrete constructions**

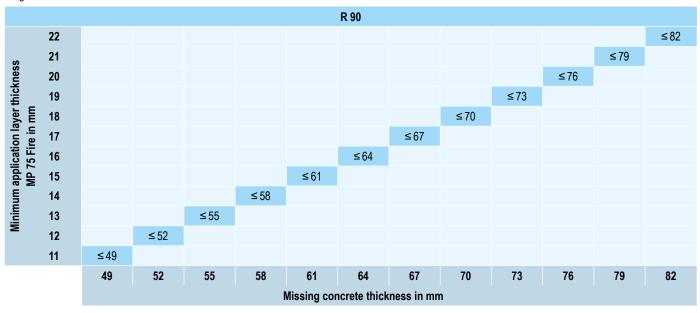
## **Columns and beams**



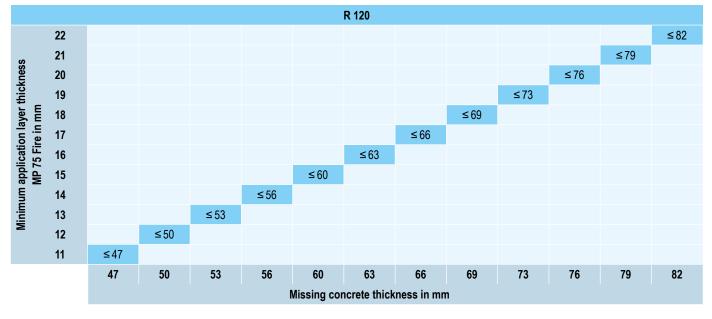
#### Minimum application layer thickness e (continuation)

In dependence on the fire resistance class and missing concrete thickness

Diagram 8



#### Diagram 9







#### Rating examples

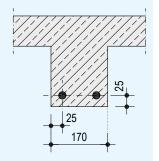
#### Concrete beams

Structurally determined supported concrete beams with simple reinforcement layer acc. to DIN EN 1992-1-2, section 5, table 5.5

Required fire resistance class: R 120 Concrete density: 2100 kg/m<sup>3</sup> Concrete strength class: C30/37 Beam width exist. b: 170 mm 25 mm Axial spacing exist. a:

Lateral axial spacing

25 mm exist. a sd: ?? mm Thickness e:



Step 1

Utilisation factor  $\mu_{fi}$  = 0.7, stressed from all sides, not prestressed acc. to DIN EN 1992-1-2, section 5, table 5.2a

Required fire

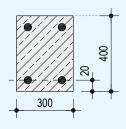
resistance class: R 90 Concrete density: 2010 kg/m<sup>3</sup> Concrete strength class: C25/30

Rectangular concrete column

300 × 400 mm Column cross-section:

Smaller column width

exist. d: 300 mm Axial spacing exist. a: 20 mm Thickness e: ?? mm



Step 1

#### Checking of the prerequisites acc. to ETA-21/0727

■ Beam width exist. b = 170 mm > 150 mm  $= 2100 \text{ kg/m}^3$ Concrete density

in range between 1955 kg/m3 to 2725 kg/m3

■ Concrete strength class = C30/37 < C50/60

Step 2

Demands on beam width and min. axial spacing acc. to DIN EN 1992-1-2, section 5, table 5.5, column 3

■ reg. b = 240 mm

■ req. a = 60 mm

■ req.  $a_{sd}$  = 60 mm + 10 mm = 70 mm

Step 3

## Deriving the missing concrete thickness

■ reg. b - exist. b = 240 mm - 170 mm = 70 mm (corresponds to 2 x 35 mm)

= 35 mm ■ req. a - exist. a = 60 mm - 25 mm ■ req. a<sub>sd</sub> - exist. a<sub>sd</sub> = 70 mm - 25 mm = 45 mm

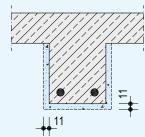
Step 4

#### Decisive missing concrete thickness

#### Deriving the min. layer thickness for MP 75 Fire

■ Diagram 9 (see page 14):

e = 11 mm



#### Checking of the prerequisites acc. to Expert Report BB-23-325-1 & -2

■ Column width exist. d = 300 mm > 80 mm

 $= 2010 \text{ kg/m}^3$ Concrete density

in range between 1955 kg/m3 to 2725 kg/m3

■ Concrete strength class = C25/30 < C30/37

Does not correspond to ETA-21/0727

#### Step 2

Demands on column width and min. axial spacing acc. to DIN EN 1992-1-2, section 5, table 5.2a, column 4

■ reg. d = 350 mm

■ req. a = 53 mm

#### Step 3

#### Deriving the missing concrete thickness

■ req. d - exist. d = 350 mm - 300 mm = 50 mm (corresponds to 2 x 25 mm)

= 33 mm ■ req. a - exist. a = 53 mm - 20 mm

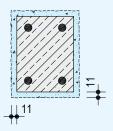
Decisive missing concrete thickness

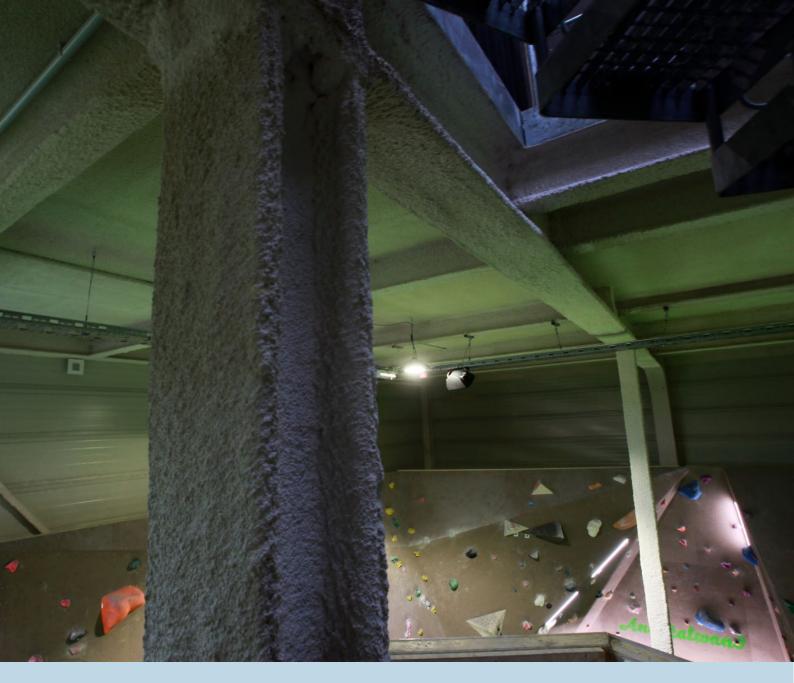
Step 4

#### Deriving the min. layer thickness for MP 75 Fire

■ Diagram 8 (see page 14):

e = 11 mm





**Steel structures** 

Fire resistant coating of steel columns and beams



#### Field of application

#### 3-sided or 4-sided exposed steel beams and columns

MP 75 Fire can be used as a fire resistant coating with the following profiles and exposure to fire.

#### **Profiles**

- I profiles
- H profiles
- L profiles
- T profiles
- U profiles
- Hollow sections
- Steel plates



- 1-sided or 2-sided exposed steel beams and columns
- Applications acc. to DIN 4102-4

The rating of the application thickness of MP 75 Fire required for fire resistance purposes on steel columns and beams is in accordance with table 3 to 6 on the pages 22 to 25 and depends on the following 3 parameters:

1. Ratio of the surface on which the heat acts (circumference) A<sub>m</sub> to the profile cross-section area V of the steel cross-section to be protected the so-called A<sub>m</sub>/V value; it is determined in accordance with page 18 taking the installation conditions into consideration.



A<sub>m</sub> = Circumference of the steel profile exposed to fire (cm)  $V = Profile\ cross-section\ (cm^2)$ 

For common profile cross-sections the A<sub>m</sub>/V values from table 2 on pages 19 to 21 can be read off.

- 2. The required fire resistance class R (retention of the stability) according to building authority requirements.
- 3. Critical steel temperature, used when dimensioning acc. to DIN EN 1993-1-2 (determined by the structural design engineer)

Protective treatment of the steel components based on alkyd resin, epoxy resin, polyurethane, zinc-dust epoxy resin or zinc-dust silicate is required.

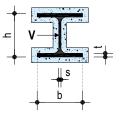
The ratio value used A<sub>m</sub>/V (profile factor) corresponds to the ratio value U/A in the DIN 4102-4 in case the cross-section remains constant over the length.

Round up the results when calculating the A<sub>m</sub>/V values.

The maximum permissible A<sub>m</sub>/V factors are 429 m<sup>-1</sup> for 3-sided exposure to flame and 495 m<sup>-1</sup> for 4-sided exposure to flame.

The maximum web height of the steel beams is 639 mm and the maximum profile height for columns is 1000 mm.

For hollow steel sections, the minimum application thickness e must be multiplied by a factor of 1.25.



- = profile width
- = hollow profile exterior diameter
- = profile height
- = web thickness
- = flange thickness or hollow profile thickness



#### Technical fire resistance assessed acc. to Experts Opinion BB-23-325-1 & -2

Prior consultation is recommended acc. to note on page 5

## **Steel structures**

## **Columns and beams**



Construction features	Exposure	A <sub>m</sub> /V in m <sup>-1</sup>	Construction features	Exposure	A <sub>m</sub> /V in m <sup>-1</sup>
b, h, s and t in cm; area V in cm <sup>2</sup>	to fire		b, h, s and t in cm; area V in cm <sup>2</sup>	to fire	
Beam or column			Hollow section, corner		
E V	All-sided	$\frac{4b + 2h - 2s}{2bt + (h - 2t) s} \cdot 100$	E D	All-sided	$\frac{2b + 2h}{(2b + 2h - 4t) t} \cdot 100$
Beam or column			Hollow section, round		
	3-sided	3b + 2h - 2s 2bt + (h - 2t) s · 100	D V	All-sided	$\frac{\pi d}{\pi t (d-t)} \cdot 100$
Beam or column			L profile		
E V	3-sided Corner	$\frac{2b + h - s}{2bt + (h - 2t) s} \cdot 100$	E b b	All-sided	$\frac{2b+2h}{bt+ht-tt} \cdot 100$
Beam or column			U profile		
b +	3-sided flange	<u>b+2t</u> · 100		3-sided	$\frac{3b + 2h - 2s}{2bt + (h - 2t) s} \cdot 100$
Flange			U profile		
b	1-side flange	Calculate complete flange thickness $\frac{b}{bt} \cdot 100$	E V D D D D D D D D D D D D D D D D D D	All-sided	4b + 2h - 2s 2bt + (h - 2t) s · 100

Note

The curves on the profile cross-sections are ignored in order to simplify calculation.



Overview  $A_m/V$  values
Table 2:  $A_m/V$  values acc. to DIN EN 1993-1-2

A <sub>m</sub> /V value in	m <sup>-1</sup> for profile							
Standard	A <sub>m</sub> /V in m <sup>-1</sup>	A <sub>m</sub> /V in m <sup>-1</sup>	Standard	A <sub>m</sub> /V in m <sup>-1</sup>	A <sub>m</sub> /V in m <sup>-1</sup>	Standard	A <sub>m</sub> /V in m <sup>-1</sup>	A <sub>m</sub> /V in m <sup>-1</sup>
DIN 1025-3	3-sided	4-sided	DIN 1025-2	3-sided	4-sided	DIN 1025-4	3-sided	4-sided
HEA 100	217.5	264.6	HEB 100	179.6	218.1	HEM 100	96.4	116.4
HEA 120	220.2	267.6	HEB 120	166.5	201.8	HEM 120	92.2	111.1
HEA 140	208.3	252.9	HEB 140	154.7	187.2	HEM 140	88.2	106.3
HEA 160	192.3	233.5	HEB 160	139.6	169.1	HEM 160	82.8	99.9
HEA 180	185.4	225.2	HEB 180	131.7	159.3	HEM 180	80.0	96.5
HEA 200	174.7	211.9	HEB 200	121.6	147.2	HEM 200	75.9	91.6
HEA 220	161.7	196.0	HEB 220	115.4	139.6	HEM 220	73.4	88.6
HEA 240	147.1	178.4	HEB 240	107.5	130.2	HEM 240	60.6	73.0
HEA 260	140.6	170.5	HEB 260	105.1	127.1	HEM 260	59.2	71.4
HEA 280	135.7	164.4	HEB 280	102.3	123.7	HEM 280	58.4	70.4
HEA 300	126.8	153.6	HEB 300	96.0	116.1	HEM 300	50.2	60.4
HEA 320	117.7	141.9	HEB 320	91.3	109.8	HEM 320/305	65.6	79.1
HEA 340	112.0	134.6	HEB 340	88.3	105.8	HEM 320	50.0	59.9
HEA 360	107.0	128.0	HEB 360	85.6	102.2	HEM 340	50.3	60.1
HEA 400	101.3	120.1	HEB 400	82.3	97.5	HEM 360	50.8	60.5
HEA 450	96.1	112.9	HEB 450	79.4	93.1	HEM 400	51.9	61.3
HEA 500	91.4	106.9	HEB 500	76.2	88.7	HEM 450	53.5	62.7
HEA 550	90.1	104.2	HEB 550	75.6	87.4	HEM 500	54.5	63.4
HEA 600	88.9	102.2	HEB 600	74.8	85.9	HEM 550	55.8	64.4
HEA 650	87.2	99.6	HEB 650	74.1	84.6	HEM 600	56.7	65.1
HEA 700	84.6	96.2	HEB 700	72.5	82.4	HEM 650	57.9	66.0
HEA 800	83.9	94.4	HEB 800	72.2	81.1	HEM 700	58.9	66.8
HEA 900	81.3	90.6	HEB 900	70.4	78.4	HEM 800	60.6	68.1
HEA 1000	80.7	89.3	HEB 1000	70.3	77.8	HEM 900	62.0	69.1
						HEM 1000	63.7	70.5

## **Columns and beams**



Overview A<sub>m</sub>/V values (continuation)
Table 2: A<sub>m</sub>/V values acc. to DIN EN 1993-1-2 (continuation)

A <sub>m</sub> /V value in m <sup>-1</sup> for pr	ofile				
Standard	A <sub>m</sub> /V in m <sup>-1</sup>	A <sub>m</sub> /V in m <sup>-1</sup>	Standard	A <sub>m</sub> /V in m <sup>-1</sup>	A <sub>m</sub> /V in m <sup>-1</sup>
DIN 1025-5	3-sided	4-sided	DIN 1025-1	3-sided	4-sided
IPE 80	369.1	429.3	IPN 80	346.1	401.6
IPE 100	335.0	388.3	IPN 100	301.9	349.1
IPE 120	311.4	359.8	IPN 120	268.3	309.2
IPE 140	291.5	336.0	IPN 140	239.6	275.8
IPE 160	269.2	310.0	IPN 160	219.7	252.2
IPE 180	254.0	292.1	IPN 180	200.0	229.4
IPE 200	234.4	269.5	IPN 200	185.3	212.3
IPE 220	221.0	253.9	IPN 220	171.4	196.2
IPE 240	205.1	235.8	IPN 240	160.1	183.1
IPE 270	197.2	226.6	IPN 260	148.8	170.0
IPE 300	187.7	215.6	IPN 280	138.9	158.4
IPE 330	174.1	199.7	IPN 300	131.2	149.3
IPE 360	162.3	185.7	IPN 320	123.4	140.3
IPE 400	152.7	174.0	IPN 340	116.8	132.6
IPE 450	143.7	163.0	IPN 360	110.0	124.7
IPE 500	132.8	150.0	IPN 380	104.8	118.7
IPE 550	124.6	140.3	IPN 400	99.6	112.7
IPE 600	114.7	128.8	IPN 450	89.1	100.7
			IPN 500	80.7	91.1
			IPN 550	75.5	84.9



Overview A<sub>m</sub>/V values (continuation)
Table 2: A<sub>m</sub>/V values acc. to DIN EN 1993-1-2 (continuation)

${\rm A_m/V}$ value in ${\rm m}^{\text{-}1}$	for profile				
Standard	A <sub>m</sub> /V in m <sup>-1</sup>	A <sub>m</sub> /V in m <sup>-1</sup>	Standard	A <sub>m</sub> /V in m <sup>-1</sup>	A <sub>m</sub> /V in m <sup>-1</sup>
DIN 1026-2	3-sided	4-sided	DIN 1026-1	3-sided	4-sided
UPE 80	290.1	339.6	U 30 x 15	398.2	466.1
UPE 100	277.6	321.6	U 30	259.2	319.9
UPE 120	259.7	298.7	U 40 x 20	333.3	388.0
UPE 140	247.3	282.6	U 40	264.1	320.5
UPE 160	234.6	266.8	U 50 x 25	317.1	367.9
UPE 180	224.7	254.6	U 50	272.5	325.8
UPE 200	212.8	240.3	U 60	286.4	332.8
UPE 220	197.9	223.0	U 65	255.8	302.3
UPE 240	187.8	211.2	U 80	242.7	283.6
UPE 270	177.9	199.1	U 100	238.5	275.6
UPE 300	153.4	171.0	U 120	222.9	255.3
UPE 330	138.3	153.8	U 140	210.3	239.7
UPE 360	129.8	143.9	U 160	200.4	227.5
UPE 400	120.0	132.5	U 180	193.2	218.2
			U 200	182.0	205.3
			U 220	170.6	192.0
			U 240	163.1	183.2
			U 260	154.0	172.7
			U 280	149.2	167.0
			U 300	145.8	163.0
			U 320	116.4	129.6
			U 350	122.9	135.8
			U 380	125.4	138.1
			U 400	116.9	129.0

## **Steel structures**

## **Columns and beams**



## Minimum application layer thickness e

In dependence on the  $A_m/V$  value, on the critical steel temperature and on the required **Fire resistance class R30** Table 3:

A <sub>m</sub> /V in m <sup>-1</sup>	R30				Critical s	teel temperat	ture in °C				
495	-	-	-	750	700	600	550	500	450	350	300
340	-	_	_	700	650	600	500	450	400	350	300
330	-	-	750	700	650	550	500	450	400	350	300
320	-	-	750	700	650	550	500	450	400	350	300
310	-	-	750	700	600	550	500	450	400	350	300
300	-	-	750	700	600	550	500	450	400	300	-
290	-	-	750	650	600	550	500	450	350	300	-
280	-	-	750	650	600	550	500	450	350	300	-
270	-	-	700	650	600	550	500	400	350	300	-
260	-	-	700	650	600	500	450	400	350	300	-
250	-	750	700	650	600	500	450	400	350	300	-
240	-	750	700	650	550	500	450	400	350	300	-
230	-	750	700	600	550	500	450	400	350	300	-
220	-	750	650	600	550	500	450	400	350	300	-
210	750	700	650	600	550	500	450	400	350	300	-
200	750	700	650	600	500	-	450	350	300	-	-
190	750	700	650	600	500	450	400	350	300	-	-
180	700	650	600	550	500	450	400	350	300	-	-
170	700	650	600	550	500	450	400	350	300	-	-
160	700	650	600	500	_	450	400	350	300	-	-
150	650	600	550	500	450	400	350	300	-	-	-
140	650	600	500	-	450	400	350	300	-	-	-
130	600	550	500	450	-	400	350	300	-	-	-
120	600	500	-	450	400	350	300	-	-	-	-
110	550	500	450	-	400	350	300	-	-	-	-
100	500	-	450	400	350	300	-	-	-	-	-
90	500	450	400	350	-	300	-	-	-	-	-
80	450	400	350	_	300	-	-	-	-	-	-
< 80	400	-	350	300	-	-	-	-	-	-	-
	10	11	12	13	13 14 15 16 17 18						20
						ım applicatio ckness e in n					

Caution

Should the determined steel temperature not be in the table, the next lower critical temperature must always be assumed.



## Minimum application layer thickness e (continuation)

In dependence on the  $A_m/V$  value, on the critical steel temperature and on the required Fire resistance class R60 Table 4:

A <sub>m</sub> /V in m <sup>-1</sup>	R60						(	Critical	steel te	mperatu	ıre in °(								
495	-	-	-	-	-	-	-	-	-	-	750	700	650	550	500	450	400	350	300
340	_	_	_	_	_	_	_	_	_	750	700	650	600	550	500	400	350	300	-
330	-	-	-	-	-	-	-	-	-	750	700	650	600	550	450	400	350	300	-
320	-	-	-	-	-	-	-	-	-	750	700	650	600	500	450	400	350	300	-
310	-	-	-	-	-	-	-	-	-	750	700	650	600	500	450	400	350	300	-
300	-	-	-	-	-	-	-	-	-	750	700	650	550	500	450	400	350	300	-
290	-	-	-	-	-	-	-	-	_	750	700	600	550	500	450	400	350	300	-
280	-	-	-	-	-	-	-	-	-	750	700	600	550	500	450	400	350	300	-
270	-	-	-	-	-	-	-	-	-	750	650	600	550	500	450	400	350	300	-
260	-	-	-	-	-	-	-	-	-	700	650	600	550	500	450	400	350	300	-
250	-	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-
240	-	-	-	-	-	-	-	-	750	700	650	600	550	450	-	400	350	300	-
230	-	-	-	-	-	-	-	-	750	700	650	600	550	450	-	400	300	-	-
220	-	-	-	-	-	-	-	-	750	700	650	600	500	450	400	350	300	-	-
210	-	-	-	-	-	-	-	-	750	700	600	550	500	450	400	350	300	-	-
200	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-	-
190	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-	-
180	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-	-
170	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-	-
160	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-	-	-
150	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-	-	-
140	-	-	-	-	-	750	700	650	600	-	550	500	450	400	350	300	-	-	-
130	-	-	-	-	-	750	700	650	600	550	500	450	400	350	-	300	-	-	-
120	-	-	-	-	750	700	650	600	-	550	500	450	400	350	300	-	-	-	-
110	-	-	-	750	700	650	-	600	550	500	450	400	-	350	300	-	-	-	-
100	-	-	750	700	650	-	600	550	500	-	450	400	350	300	-	-	-	-	-
90	750	-	700	650	-	600	550	500	-	450	400	350	300	-	-	-	-	-	-
80	700	-	650	600	-	550	500	-	450	400	350	-	300	-	-	-	-	-	-
< 80	650	-	-	600	550	500	-	450	400	-	350	300	-	-	-	-	-	-	-
	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28
							Mini	mum ap		on layer mm	thickne	ess e							

in mm

Caution Should the determined steel temperature not be in the table, the next lower critical temperature must always be assumed.

## **Steel structures**

## Columns and beams



## Minimum application layer thickness e (continuation)

In dependence on the  $A_m/V$  value, on the critical steel temperature and on the required **Fire resistance class R90** Table 5:

A <sub>m</sub> /V in m <sup>-1</sup>	R90 Critical steel temperature in °C																			
495	-	-	-	-	-	-	-	-	-	-	-	750	700	650	550	500	450	400	350	300
340	-	-	-	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300
330	-	-	-	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300
320	_	-	_	_	-	_	_	-	-	-	750	700	650	600	550	500	450	400	350	300
310	-	-	-	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300
300	-	-	-	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300
290	-	-	-	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300
280	-	-	-	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300
270	-	-	_	-	-	-	-	-	-	-	750	700	650	550	500	450	400	350	300	-
260	-	-	-	-	-	-	-	-	-	-	750	700	600	550	500	450	400	350	300	-
250	-	-	-	-	-	-	-	-	-	-	700	650	600	550	500	450	400	350	300	-
240	-	-	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-
230	-	-	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-
220	-	-	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-
210	-	-	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-
200	-	-	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-
190	-	-	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-
180	-	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-	-
170	-	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-	-
160	-	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-	-
150	-	-	-	-	-	-	-	750	700	-	650	600	550	500	450	400	350	300	-	-
140	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	-	300	-	-
130	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-	-	-
120	-	-	-	-	-	-	750	700	650	600	550	-	500	450	400	350	300	-	-	-
110	-	-	-	-	-	750	700	-	650	600	550	500	450	400	350	300	-	-	-	-
100	-	-	-	-	750	-	700	650	600	550	500	-	450	400	350	300	-	-	-	-
90	-	-	-	750	700	650	650	600	550	-	500	450	400	350	300	-	-	-	-	-
80	-	750	-	700	650	-	600	550	-	500	450	400	350	300	-	-	-	-	-	-
< 80	750	-	700	650	-	600	550	-	500	450	400	-	350	300	-	-	-	-	-	-
	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35
								Mi	nimum thickr	applica ness e i		yer								

Caution

Should the determined steel temperature not be in the table, the next lower critical temperature must always be assumed.



## Minimum application layer thickness e (continuation)

In dependence on the  $A_m/V$  value, on the critical steel temperature and on the required **Fire resistance class R120** Table 6:

A <sub>m</sub> /V in m <sup>-1</sup>	R120						Crit	ical stee	el tempe	rature ir	ı °C							
495	-	-	-	_	-	-	-	-	750	700	650	600	550	500	450	400	350	300
340	_	-	_	_	_	_	_	750	700	650	600	550	500	450	400	350	-	300
330	_	-	_	_	_	_	_	750	700	650	600	550	500	450	400	350	300	-
320	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-
310	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-
300	-	-	-	-	-	-	_	750	700	650	600	550	500	450	400	350	300	-
290	-	-	_	-	-	-	_	750	700	650	600	550	500	450	400	350	300	-
280	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-
270	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-
260	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-
250	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-
240	-	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-
230	-	-	-	_	-	-	750	700	650	600	550	-	500	450	400	350	300	-
220	-	-	-	_	-	-	750	700	650	600	550	500	450	-	400	350	300	-
210	-	-	-	_	-	-	750	700	650	600	550	500	450	400	350	-	300	-
200	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-	-
190	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	_	-
180	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	_	-
170	-	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-	-
160	-	-	-	-	-	750	700	650	600	550	-	500	450	400	350	300	-	-
150	-	-	-	-	-	750	700	650	600	550	500	450	400	350	-	300	-	-
140	-	-	-	-	-	750	700	650	600	550	500	450	400	350	300	-	-	-
130	-	-	-	-	750	-	700	650	600	550	500	450	400	350	300	-	-	-
120	-	-	-	-	750	700	650	600	550	500	450	-	400	350	300	-	-	-
110	-	-	-	750	-	700	650	600	550	500	450	400	350	300	-	-	-	-
100	-	-	-	750	700	650	600	550	500	-	450	400	350	300	-	-	-	-
90	-	-	750	700	650	-	600	550	500	450	400	350	300	-	-	-	-	-
80	_	750	700	650	-	600	550	500	450	400	350	300	-	-	-	-	-	-
< 80	750	700	650	-	600	550	500	450	-	400	350	300	-	-	-	-	-	-
	26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43																	
	Minimum application layer thickness e in mm																	

thickness e in mm

**Caution** Should the determined steel temperature not be in the table, the next lower critical temperature must always be assumed.

#### Steel structures

#### Columns and beams



#### **Rating examples**

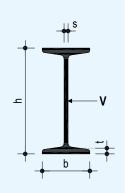
#### I profile

Profile: I 200
Critical steel temperature: 500° C

Cross-sectional dimensions

h: 20 cm
b: 9 cm
s: 0.75 cm
t: 1.13 cm
Required

fire resistance class: R 90
Fire exposure: 3-sided
Thickness e: ?? mm



Step 1

#### **Hollow profile**

Profile: 160 × 90 × 8 mm

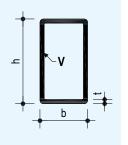
Critical steel temperature: 750° C

Cross-sectional dimensions

■ h: 16 cm ■ b: 9 cm ■ t: 0.8 cm

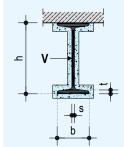
Required

fire resistance class: R 120
Fire exposure: All-sided
Thickness e: ?? mm



Step 1

## Determination of A<sub>m</sub>/ V values for steel columns and beams



#### 3-sided

$$A_{m}/V = \frac{3b + 2h - 2s}{2bt + (h - 2t) s} \cdot 100$$

$$A_{m}/V = \frac{3.9 + 2.20 - 2.0.75}{2.9.1.13 + (20 - 2.1.13) \cdot 0.75} \cdot 100$$

$$A_{\rm m}/V = \frac{65.50}{33.645} \cdot 100$$

$$A_{\rm m}/V = 194.68 \text{ m}^{-1}$$

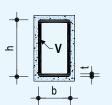
Condition for use of table 5 on page 24 fulfilled:

 $A_{\rm m}/V$  value: 194.68 m<sup>-1</sup>  $\leq$  429 m<sup>-1</sup>

Step 2

## Determination of $A_m/V$ values for steel columns and beams

4-sided



$$A_m/V = \frac{2b + 2h}{(2b + 2h - 4t)t} \cdot 100$$

$$A_{m}/V = \frac{2 \cdot 9 + 2 \cdot 16}{(2 \cdot 9 + 2 \cdot 16 - 4 \cdot 0.8) \cdot 0.8} \cdot 100$$

$$A_{m}/V = \frac{50}{37.44} \cdot 100$$

 $A_m/V = 133.55 \text{ m}^{-1}$ 

Condition for use of table 6 on page 25 fulfilled:

 $A_{m}/V$  value:  $133.55 \text{ m}^{-1} \le 495 \text{ m}^{-1}$ 

Step 2

#### Minimum application layer thickness e

A <sub>m</sub> /V value in m <sup>-1</sup>	R 90 Critical steel temperature in °C									
230	600	550	500	450	400					
220	600	550	500	450	400					
210	600	550	500	450	400					
200	600	550	500	450	400					
190	600	550	500	450	400					
180	550	500	450	400	350					
170	550	500	450	400	350					
	28	29	30	31	32					

Minimum application layer thickness e in mm

For the A<sub>m</sub>/V value the same or next higher value from table 5 on page 24 must be determined.

Result

Minimum application thickness MP 75 Fire: ≥ 30 mm

#### Minimum application layer thickness e

A <sub>m</sub> /V value in m <sup>-1</sup>	R 120 Critical steel temperature in °C									
170	-	-	-	750	700					
160	-	-	750	700	650					
150	-	-	750	700	650					
140	-	-	750	700	650					
130	-	750	-	700	650					
120	-	750	700	650	600					
110	750	-	700	650	600					
	29	30	31	32	33					

Minimum application layer thickness e in mm

For the  $A_{\rm m}N$  value the same or next higher value from table 6 on page 25 must be determined.

Result × 1.25 (25 % safety margin)

Minimum application thickness MP 75 Fire: 1.25 × 31 mm ≥ 39 mm



# **Special constructions**Fire resistance coating of

Ribbed ceilings without intermediate components
Ribbed ceilings with intermediate components
Reinforced concrete hollow ceilings
Brick and brick/steel ceilings
Vaulted ceilings

Hollow clay element ceiling

Concrete ceilings with embedded steel beams (coves)

## **Special constructions**

## Ribbed ceilings without intermediate components





#### Field of application

# 1-sided exposed concrete ceilings and 3-sided or 4-sided exposed concrete beams and columns

- For a concrete density in a range of 1955 kg/m³ to 2725 kg/m³
- Beam width of at least 150 mm
- Beam height of at least 450 mm
- Concrete strength class C30/37 up to and including C50/60

## plus

- Beam width of 80 149 mm
- Concrete density in a range of 800 kg/m<sup>3</sup> to 1954 kg/m<sup>3</sup>
- Concrete classes < C30/37
- Applications acc. to DIN 4102-4
- Fire resistance classes 30 to 180 minutes

The rating of the application thickness of MP 75 Fire required for fire resistance purposes on concrete components is in accordance with the tables on pages 8 to 10 and depends on

- Constructional component and loading
- Required fire resistance class according to building authority requirements
- Demands on the concrete thickness acc. to DIN EN 1992-1-2, section 5 for the necessary fire resistance class
- Existing concrete thickness
- Equivalent thickness of concrete of the ETA-21/0727

#### **Procedure**

- 1. Observe the fields of application.
- 2. Determine the required thicknesses, width and minimum spacings of concrete acc to DIN EN 1992-1-2, section 5.
- 3. Determine existing concrete thickness, width and minimum spacings and derive the decisive (maximum) missing concrete thickness.
- Read off the minimum plaster layer thickness e for MP 75 Fire in accordance with the missing concrete thickness from the tables on pages 8 to 10.

For rating examples see the following page.

#### **Downstand beams**

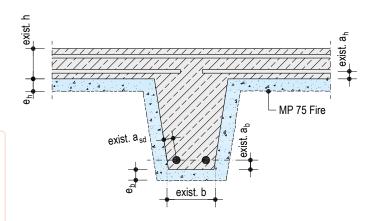
The downstand beams of ribbed ceilings can be fire resistance upgraded with MP 75 L Fire in acc. with the indicated equivalent concrete thicknesses for concrete beams and supports in ETA-21/0727.

The application thicknesses from diagrams 6 to 10 on pages 13 and 14 apply.

#### Slab area

The slab area of the ribbed ceiling is considered separately and fire resistance upgraded in acc. with the equivalent concrete thickness for concrete covers.

The application thicknesses from diagrams 1 to 5 on pages 8 to 10 apply.



exist. a<sub>h</sub> = existing axial spacing in the downstand beam

exist. a<sub>h</sub> = existing axial spacing in the cover

exist. a<sub>sd</sub> = existing axial spacing in the downstand beams

exist. b = existing rib width in the height of the centre of gravity of the tensile area reinforcement

exist. h = available cover thickness

**e.** = thickness MP 75 Fire on the downstand beams

**e**<sub>h</sub> = thickness MP 75 Fire in flat section



Technical fire resistance assessed acc. to Experts Opinion BB-23-325-1 & -2

■ Prior consultation is recommended acc. to note on page 5

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## Ribbed ceilings without intermediate components

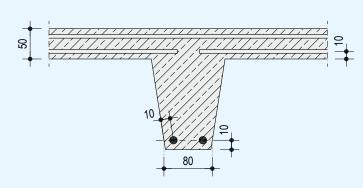
#### Rating example

Twin-axis stressed structurally determined supported reinforced concrete ribbed ceiling with simple reinforcement layer acc. to **DIN EN 1992-1-2, section 5, table 5.10** 

Required fire resistance class: **REI 90** Concrete density: 2010 kg/m<sup>3</sup> Concrete strength class: C30/37 Existing cover thickness exist. h: 50 mm Existing axial spacing concrete cover exist. a,: 10 mm Existing rib width exist. b: 80 mm Existing rib axial spacing exist. a<sub>h</sub>: 10 mm

Existing rib lateral axial spacing

10 mm exist. a sd: Thickness  $e_b$  and  $e_h$ : ?? mm



Step 1

#### Checking of the prerequisites acc. to Expert Opinion BB-23-325-2

Rib width exist. b = 80 mm ≥ 80 mm

= 2010 kg/m<sup>3</sup> corresponds to normal-weight concrete acc. to DIN EN 206-1 / DIN 1045-2 Concrete density

 Concrete strength class = C30/37 corresponds with ETA-21/0727

Step 2 Step 2

#### Downstand beam with simple reinforcement layer

Demands on rib width and minimum spacings acc. to DIN EN 1992-1-2, section 5, table 5.10, column 3

- req. b = 160 mm
- req. a<sub>b</sub> = 40 mm
- req. a<sub>sd</sub> = 40 mm + 10 mm = 50 mm

#### Step 3

#### Deriving the missing concrete thickness

- req. b req. b = 160 mm 80 mm
- req.  $a_b$  exist.  $a_b$  = 40 mm 10 mm

Decisive missing concrete thickness

Step 4

= 80 mm (corresponds to 2 x 40 mm)

= 30 mm

 $\blacksquare$  req.  $a_{sd}$  - exist.  $a_{sd}$  = 50 mm - 10 mm = 40 mm

Reading off the min. application thickness e<sub>h</sub> for MP 75 Fire

■ Diagram 8 (see page 14):

e<sub>b</sub> = 11 mm

#### **Board area**

Demands on board thickness and minimum spacings acc. to DIN EN 1992-1-2, section 5, table 5.10, column 5

- req. h = 100 mm
- req. a<sub>h</sub> = 15 mm

#### Step 3

#### Deriving the missing concrete thickness

- req. h exist. h = 100 mm 50 mm = 50 mm
- req. a<sub>h</sub> exist. a<sub>h</sub> = 15 mm 10 mm = 5 mm

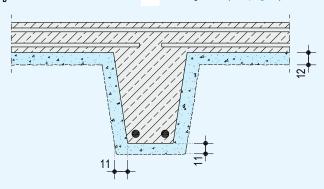
Decisive missing concrete thickness = 50 mm

Step 4

## Read off min. layer thickness e<sub>h</sub> for MP 75 Fire

■ Diagram 3 (see page 9):

e<sub>h</sub> = 12 mm



## **Special constructions**

## Ribbed ceilings with intermediate components





#### Field of application

Figure 1: Intermediate component acc. to DIN EN 15037-3, type SR

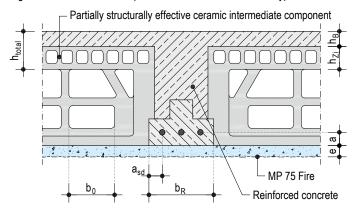
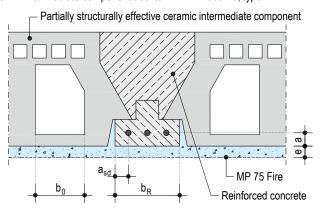


Figure 2: Intermediate component acc. to DIN EN 15037-3, type RR



**A**<sub>Net</sub> = net cross-section area of the intermediate components

a = vertical axial spacing

a<sub>sd</sub> = lateral axial spacing

 $b_{R}$  = rib width

**b**<sub>0</sub> = spacings of intermediate component internal webs

h<sub>B</sub> = thickness of applied concrete

 $m{h}_{ ext{total}}$  = effective fire protection cover thickness  $m{h}_{ ext{Int}}$  = creditable height of brick lay-in ceiling

e = thickness MP 75 Fire

Figure 3: Intermediate component acc. to DIN EN 15037-2 with level bottom

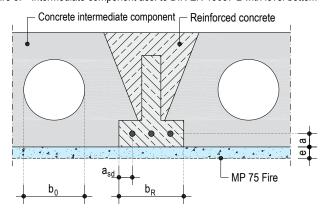
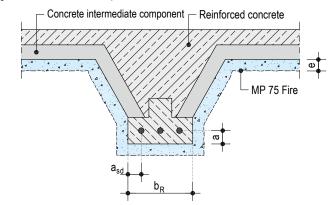


Figure 4: Intermediate component acc. to DIN EN 15037-2 with non-level bottom



MP 75 Fire in accordance with the specifications of the Expert Opinion BB-23-325-2 or. DIN 4102-4:2016-05 can be applied on intermediate components made of concrete or ceramic intermediate components (acc. to DIN EN 15037-2 and 3).

Initially, the suitability of the existing cover must be certified for the required fire resistance class to the requirements in the DIN 4102-4:2016-05.

#### Case 1: Level bottom (Figure 1 - 3)

The reinforced concrete ribs can be reinforced with MP 75 Fire n accordance with the equivalent concrete thicknesses specified for concrete ceilings and walls (diagram 1 to 5 from page 8 ff.).

#### Preconditions:

- $\blacksquare$  h = A<sub>Net</sub>/b
- $b_0 \le 60 \text{ mm (for type RR)}$
- Further requirements: see DIN 4102-4:2016-05, section 5.7

#### Case 2: Non-level bottom (Figure 4)

The reinforced concrete ribs can be reinforced with MP 75 Fire in accordance with the equivalent concrete thicknesses specified for concrete beams and columns (diagram 6 to 10 from page 13 ff.).

#### **Preconditions:**

- w≥80 mm
- Further requirements: see DIN 4102-4:2016-05, section 5.7



# Technical fire resistance assessed acc. to Experts Opinion BB-23-325-1 & -2

■ Prior consultation is recommended acc. to note on page 5

## Ribbed ceilings with intermediate components

#### Rating example

Reinforced concrete ribbed ceiling with intermediate component of type RR - DIN 4102-4:2016-05, Tab.5.14, lines 1.1.2, 2 and 3.1

Required fire resistance class: REI 90

Concrete density: 2010 kg/m³

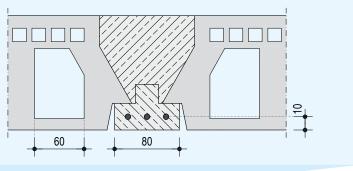
Effective ceiling thickness  $h_{total}$ : 80 mm

Existing rib width  $w_R$ : 80 mm

Spacing of intermediate component web  $b_0$ : 60 mm

Existing axial spacing a: 10 mm

Thickness e: ?? mm



Step 1

#### Checking of the prerequisites

■ exist. lap width  $w_0$ : = 60 mm ≤ 60 mm

■ Calculation of  $h_{total}$  from  $h_{zi}$ ,  $h_B$  and  $A_{Net}$  acc. to DIN 4102-4, section 5.7.2

■ Concrete density = 2010 kg/m³ corresponds to normal-weight concrete acc. to DIN EN 206-1 / DIN 1045-2

■ Concrete strength class C25/30 < C50/60

#### Step 2

#### Requirements on the total thickness (ribs intermediate components)

Definition of the minimum requirements on the ceiling height  $h_{total}$ , rib width  $b_R$  and min. axial spacing a acc. to DIN 4102-4:2016-05, table 5.14, lines 1.1.2, 2 and 3.1 or acc. to DIN EN 1992-1-2:2010-12, table 5.8, columns 2 and 3

■ req. h<sub>total</sub>= 100 mm

■ req. b<sub>R</sub> = no requirement

■ req. a = 30 mm

#### Step 3

#### Deriving the missing concrete thickness

■ req. h<sub>total</sub> - exist. h<sub>total</sub> = 100 mm - 80 mm = **20 mm** 

■ req. w<sub>R</sub>: Must not be considered

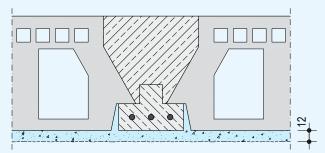
■ req. a - exist. a = 30 mm - 10 mm = 20 mm

Decisive missing concrete cover = 20 mm

#### Step 4

## Deriving the min. layer thickness for MP 75 Fire

■ Diagram 3 (see page 9):



e = 12 mm

## **Special constructions**

## Reinforced concrete hollow ceilings



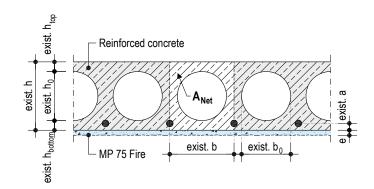


#### Field of application

Reinforced concrete slabs with cavities can be upgraded acc. to the Experts Opinion BB-23-325-2 and the specifications acc. to DIN 4102-4:2016-05. For fire resistance upgrading with MP 75 Fire, the equivalent concrete thicknesses from chapter "Ceilings and walls" (diagrams 1 to 5 from page 8 ff.) must be considered.

Preconditions acc. to Experts Opinion BB-23-325-2 and/or DIN 4102-4:2016-05

- For reinforced concrete slabs with plemums  $(w_0/h_0 > 1)$  see DIN 4102-4:2016-05, section 5.4:
  - A<sub>Net</sub>/w ≥ h
  - exist. h<sub>bottom</sub> ≥ 50 mm
- For reinforced concrete hollow slabs with plemums ( $w_0/h_0 > 1$ ) see DIN 4102-4:2016-05, section 5.5:
  - exist. a ≥ 10 mm
  - exist. h ≥ 80 mm



 A<sub>Net</sub>
 = net cross-section area

 exist. a
 = existing axial spacing

 exist. b
 = existing cross-section width

 exist. b<sub>0</sub>
 = existing plenum width

 exist. h
 = existing slab thickness

**exist.**  $h_{top}$  = existing concrete thickness above plenum **exist.**  $h_{bottom}$  = existing concrete thickness below plenum

exist. h<sub>0</sub> = existing plenum height e = thickness MP 75 Fire

Technical fire resistance assessed acc. to Experts Opinion BB-23-325-1 & -2

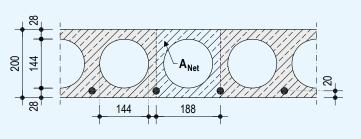
■ Prior consultation is recommended acc. to note on page 5



#### Rating example

Rating example – Raw reinforced concrete hollow core slabs made of normal concrete  $b_0/h_0 \le 1$ , regardless of the arrangement of a screed with the same bar diameters in accordance with DIN 4102-4:2016-05, tables 5.7 line 4 (or 1.1) and 5.8 line 2 (or 1.1)

Required fire resistance class: **REI 90** Concrete density: 2010 kg/m<sup>3</sup> Concrete strength class: C45/55 Existing ceiling thickness exist. h: 200 mm Plenum height h<sub>0</sub>: 144 mm Plenum width b<sub>0</sub>: 144 mm Axial spacing exist. a: 20 mm Thickness e: ?? mm



Step 1

#### Checking of the prerequisites

■  $w_0/h_0$  = 144 mm/144 mm ≤ 1 ■ exist. h = 200 mm > 80 mm ■ exist. a = 20 mm > 10 mm

■ Concrete density = 2010 kg/m³ corresponds to normal-weight concrete acc. to DIN EN 206-1 / DIN 1045-2

■ Concrete strength class C45/55 < C50/60

#### Step 2

## Demands on cover thickness and minimum spacing acc. to DIN 4102-4:2016-05, tables 5.7 and 5.8

req. h = 120 mmreq. a = 35 mm

Step 3

#### Deriving the missing concrete thickness

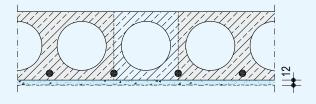
■ req. h - exist. h = 120 mm - 200 mm = -80 mm = req. a - exist. a = 35 mm - 20 mm = 15 mm

Decisive missing concrete cover = 15 mm

#### Step 4

#### Deriving the min. layer thickness for MP 75 Fire

■ Diagram 3 (see page 9): e = 12 mm



## **Special constructions**

## Brick and brick/steel ceilings



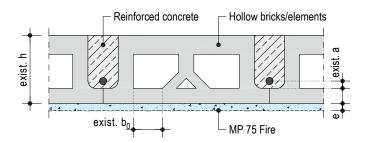


#### Field of application

MP 75 Fire can be used in accordance with the specifications of the Expert Opinion BB-23-325-2 or. DIN 4102-4:2016-05 on brick ceilings acc. to DIN EN 1045-2-100). The brick ceilings (brick/steel ceilings) can be reinforced with MP 75 Fire in accordance with the equivalent concrete thicknesses specified for concrete ceilings and walls (diagram 1 to 5 from page 8 ff.).

#### Requirements:

- For REI  $\geq$  60 only floor bricks acc. to DIN 4159 maybe used, where the clearances  $b_0$  of the vertical or inclined internal webs  $b_0 \leq$  60 mm.
- For the minimum thickness h of the brick ceiling DIN 4102-4:2016-05, table. 5.15, line 1.1, must be consulted.
- The minimum spacing a is assessed differently depending on the mounting and column width in accordance with DIN 4102-4:2016-05, table. 5.15, lines 2.1 to 2.2.3.



exist. a = existing axial spacing

**exist.**  $b_0$  = existing spacings of the brick internal webs

exist. h = existing slab thickness e = thickness MP 75 Fire



Technical fire resistance assessed acc. to Experts Opinion BB-23-325-1 & -2

■ Prior consultation is recommended acc. to note on page 5

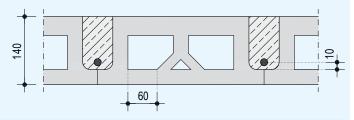




## Brick and brick/steel ceilings

#### Rating example

#### Brick ceiling acc. to DIN 1045-100 - structurally determined, wit consideration of a screed



Step 1

#### Checking of the prerequisites

■ exist. lap width  $w_0$ : = 60 mm ≤ 60 mm

#### Step 2

#### Rating of the brick ceiling

Definition of the minimum requirements on the ceiling height h and minimum axial spacing a acc. to DIN 4102-4:2016-05, table 5.15, lines 1.1 and 2.1

- req. h = 165 mm
- req. a = 20 mm

#### Step 3

#### Deriving the missing concrete thickness

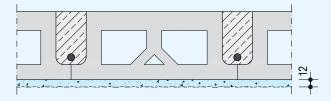
■ req. h - exist. h = 165 mm - 140 mm = 25 mm ■ req. a - exist. a = 20 mm - 10 mm = 10 mm Decisive missing concrete cover = 25 mm

#### Step 4

#### Deriving the min. layer thickness for MP 75 Fire

■ Diagram 3 (see page 9):

e = 12 mm



## **Special constructions**

## **Vaulted ceilings**





#### Field of application

MP 75 Fire can be used directly on vaulted ceilings and without plaster bases. The plaster can be applied fully or only partially in the area of the underflange.

The specifications of the Expert Opinion BB-23-325-2 or DIN 4102-4:1994-03, section 3.11.3 apply.

#### Rating of the application thickness on steel

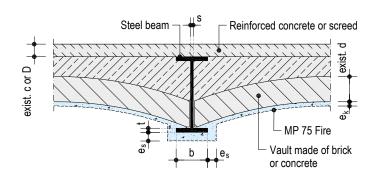
- Determination of the A<sub>m</sub>/V value of the steel beam section to be protected:
- Steel area exposed to flame (V) = cross-section of the lower flange
- Circumference (A<sub>m</sub>) = circumference of the actual (generally 4-sided) exposed to flame, freely-exposed flange section (see example on the following page)
- Read off the application thickness from the tables (tables 3 to 6) from page 22

#### Rating of the application thickness above the ceiling sections (vaults)

- The specifications of the minimum thicknesses D and c acc. to DIN 4102-4:1994-03, table 29, lines 1.2 and 1.3, must be observed.
- Determination of the required vault thickness d acc. to DIN 4102-4:1994-03, table 29, line 1.1.
- Rating of the missing vault thickness: d<sub>req</sub> d<sub>exist</sub>
- Reinforcement with MP 75 Fire in accordance with the equivalent concrete thicknesses specified for concrete slabs and walls (diagram 1 to 5 from page 8 ff.).

Caution

The steel beam must be covered on 3 sides with the determined application thickness and the transition between steel and vaulted ceiling must be filled out.



**b** = beam width

exist. c = existing concrete cover over the steel beam

exist. D = existing screed thicknessexist. d = existing vault thickness

s = web thicknesst = flange thickness

e<sub>k</sub> = application thickness MP 75 Fire over the vault
 e<sub>s</sub> = application thickness MP 75 Fire over the steel

Technical fire resistance assessed acc. to Experts Opinion BB-23-325-1 & -2

■ Prior consultation is recommended acc. to note on page 5





#### Rating example

Thickness e<sub>k</sub>:

#### Prussian vaulted ceiling with I 300 beam, brick masonry and concrete layer Required fire resistance class: **REI 120** 500°C Critical steel temperature: Beam width b: 125 mm Web thickness s: 10.8 mm Flange thickness t: 16.2 mm Exposed steel top (flange) 10 mm Vault thickness d: 100 mm Concrete layer c: 50 mm ?? mm Thickness e<sub>s</sub>:

Step 1

#### Checking of the prerequisites acc. to DIN 4102-4:1994-03, table 29, lines 1.2 and 1.3

No screed required, as

exist. c = 50 mm ≥ 45 mm

#### Step 2

#### Calculation of the application thickness above the ceiling sections (vaults)

- Determination of the required vault thickness d acc. to DIN 4102-4:1994-03, table 29, line 1.1 d<sub>req</sub> = 120 mm
- Determination of the missing vault thickness:

?? mm

 $d_{req} - d_{exist} = 120 \text{ mm} - 100 \text{ mm} = 20 \text{ mm}$ 

■ Determination of the required application thickness (see diagram 4 on page 9)

e<sub>k</sub> = 12 mm

#### Step 3

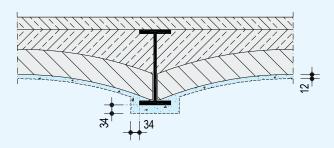
#### Calculation of the application thickness above the steel beam sections

- A<sub>m</sub>/V value calculation
- $A_m = b + 2t + 2 \cdot 10 = 125 \text{ mm} + 2 \cdot 16.2 \text{ mm} + 2 \cdot 10 \text{ mm} = 177.4 \text{ mm} = 17.74 \text{ cm}$
- $V = b \cdot t = 125 \text{ mm} \cdot 16.2 \text{ mm} = 2025 \text{ mm}^2 = 20.25 \text{ cm}^2$
- $A_m/V = (17.74 \text{ cm} / 20.25 \text{ cm}^2) \cdot 100 \sim 90 \text{ m}^{-1}$
- Determination of application thickness at R120, 500 °C (see table 6 on page 25)

e<sub>s</sub> = 34 mm

#### Step 4

#### Definition of application thickness execution



## **Special constructions**

## Hollow clay element ceilings





#### Field of application

MP 75 Fire can be used directly on hollow clay element ceilings and without plaster bases. The plaster can be applied fully or only partially in the area of the underflange.

The specifications of the Expert Opinion BB-23-325-2 or DIN 4102-4:1994-03, section 3.11.3 apply.

#### Rating of the application thickness on steel

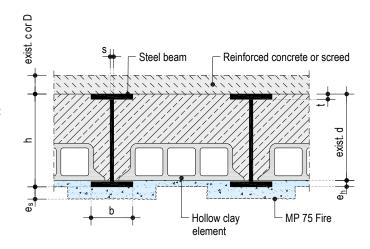
- Determination of the A<sub>m</sub>/V value of the steel beam section to be protected:
- Steel area exposed to flame (V) = cross-section of the lower flange
- Circumference (A<sub>m</sub>) = circumference of the actual (generally 3-sided) exposed to flame, freely-exposed flange section (see example on the following page)
- Read off the application thickness from the tables (tables 3 to 6) from page 22

# Rating of the application thickness above the ceiling sections (hollow clay elements)

- The specifications of the minimum thicknesses D and c acc. to DIN 4102-4:1994-03, table 29, lines 1.2 and 1.3, must be observed.
- Calculation of the effective fire protection cover thickness t: t = A.../b
- Determination of the required min. thickness d acc. to DIN 4102-4:1994-03, table 29, line 1.1.
- Rating of the missing vault thickness: d<sub>req</sub> d<sub>exist</sub>
- Reinforcement with MP 75 Fire in accordance with the equivalent concrete thicknesses specified for concrete slabs and walls (diagram 1 to 5 from page 8 ff.).

Caution

The steel beam must have a lateral overlap of at least 50 mm covered by the determined application thickness.



A<sub>Net</sub> = net cross-section area

**b** = beam width

**exist. c** = existing concrete cover over the steel beam

exist. D = existing screed thickness

exist. d = existing fire protection cover thickness

h = beam height
 s = web thickness
 t = flange thickness

**e**<sub>s</sub> = application thickness MP 75 Fire over the steel

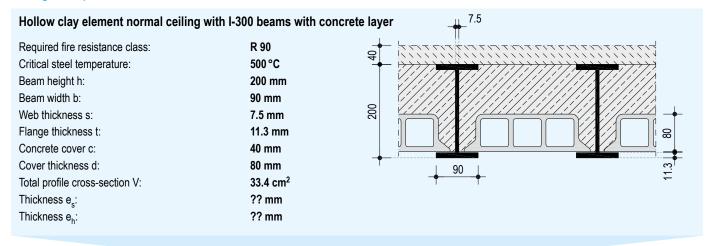
**e**<sub>h</sub> = application thickness MP 75 Fire over the hollow clay element

Technical fire resistance assessed acc. to Experts Opinion BB-23-325-1 & -2

■ Prior consultation is recommended acc. to note on page 5



#### Rating example



Step 1

#### Checking of the prerequisites acc. to DIN 4102-4:1994-03, table 29, lines 1.2 and 1.3

■ No screed required, as

exist. c = 40 mm ≥ 35 mm

#### Step 2

#### Determination of the application thickness above the ceiling sections (hollow clay elements)

- Comparison of the effective fire protection cover thickness t: (= A<sub>Net</sub>/b) with the specifications acc. to DIN 4102-4:1994-03, table 29, line 1.1.
  - t<sub>req</sub> = 100 mm
  - t<sub>exist</sub> = 80 mm
  - $t_{req} t_{exist}$  = 100 mm 80 mm = 20 mm

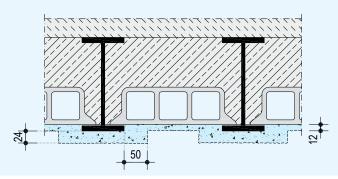
#### Step 3

#### Calculation of the application thickness above the steel beam sections

- A<sub>m</sub>/V value calculation
  - A<sub>m</sub> = b + 2t = 90 mm + 2 · 11.3 mm = 112.6 mm = 11.3 cm
  - V = 33.4 cm<sup>2</sup>
  - $A_m/V = (11.3 \text{ cm} / 33.4 \text{ cm}^2) \cdot 100 = 33.8 \text{ m}^{-1} \le 80.0 \text{ m}^{-1}$
- Determination of application thickness at R 90, 500 °C (see table 5 on page 24) e<sub>s</sub> = 24 mm

#### Step 4

#### Definition of application thickness execution



## **Special constructions**

## Concrete ceilings with embedded steel beams (arched ceiling)





#### Field of application

MP 75 Fire can be used on arched ceilings or similar concrete ceilings with embedded steel beams.

The specifications of the Expert Opinion BB-23-325-2 or DIN 4102-4:1994-03, section 3.11.2 apply.

#### Rating of the application thickness on steel

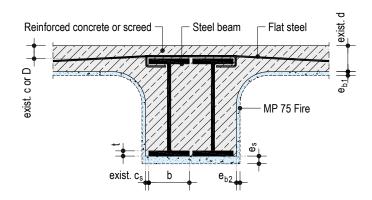
- Determination of the A<sub>m</sub>/V value of the steel beam section to be protected:
  - Steel area exposed to flame (A<sub>m</sub>) = cross-section of the lower flange
  - Profile cross-section (V) = circumference of the actual freely-exposed flange section (see example on the following page)
- Read off the application thickness from the tables (tables 3 to 6) from page 22

#### Rating of the application thickness on concrete

- The specifications of the minimum thicknesses D and c acc. to DIN 4102-4:1994-03, table 29, lines 1.2 and 1.3, must be observed.
- Determination of the required min. thickness d acc. to DIN 4102-4:1994-03, table 29, line 1.1.
- Rating of the missing minimum thickness for the ceiling area:
   d<sub>rea</sub> d<sub>exist</sub>
- Reinforcement with MP 75 Fire (e<sub>b1</sub>) in accordance with the equivalent concrete thicknesses specified for concrete slabs and walls (diagram 1 to 5 from page 8 ff.).
- Determination of the required min. concrete thickness c<sub>s</sub> acc. to DIN 4102-4:1994-03, table 29, line 2.1.1.1 or 2.1.2.1.
- Rating of the missing concrete cover laterally on the beam: req. c<sub>s</sub> - exist. c<sub>s</sub>
- Reinforcement with MP 75 Fire (e<sub>b2</sub>) in accordance with the equivalent concrete thicknesses specified for concrete supports and beams (diagram 6 to 10 from page 13 ff.).



Different and diverse requirements and ratings apply for the exposed steel, the concrete cover thickness and the lateral concrete cover of the downstand beams.



**b** = beam width

**exist.**  $\mathbf{c}$  = existing concrete cover over the steel beam **exist.**  $\mathbf{c}_{\mathbf{s}}$  = lateral concrete cover over the steel beam

exist. D = screed thickness

exist. d = cover thickness (outside the beam area)

t = flange thickness

 $\mathbf{e_{b1}}$  = application thickness MP 75 Fire over the concrete  $\mathbf{e_{b2}}$  = application thickness MP 75 Fire laterally from the

downstand beam

**e**<sub>s</sub> = application thickness MP 75 Fire over the steel



Technical fire resistance assessed acc. to Experts Opinion BB-23-325-1 & -2

■ Prior consultation is recommended acc. to note on page 5

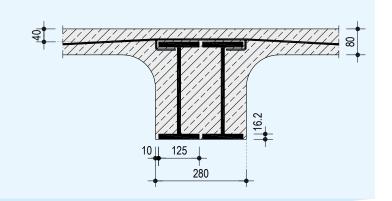


## Concrete ceilings with embedded steel beams (arched ceiling)

#### Rating example

#### Half-dome arched ceiling with I-300 beams

Required fire resistance class: **REI 90** Critical steel temperature: 500°C Beam width b: 125 mm Flange thickness t: 16.2 mm Concrete cover c: 40 mm Cover thickness d: 80 mm Lateral concrete cover on the steel beam c<sub>s</sub>: 10 mm ?? mm Thickness e.: ?? mm Thickness e<sub>h1</sub>: Thickness e<sub>b2</sub>: ?? mm



Step 1

#### Checking of the prerequisites acc. to DIN 4102-4:1994-03, table 29, lines 1.2 and 1.3

■ No screed required, as

exist.  $c = 40 \text{ mm} \ge 35 \text{ mm}$ 

#### Step 2

#### Calculation of the application thickness on the concrete cover

- Comparison of the cover thickness d with the specifications acc. to DIN 4102-4:1994-03, table 29, line 1.1.:
  - t<sub>req</sub> = 100 mm
  - t<sub>exist</sub> = 80 mm
- t<sub>req</sub> t<sub>exist</sub> = 100 mm 80 mm = 20 mm
- Determination of the required application thickness (see diagram 3 on page 9) 
   b<sub>b1</sub> = 12 mm

#### Step 3

#### Determination of the application thickness laterally from the downstand beam

- Comparison of the lateral concrete cover with the specifications acc. to DIN 4102-4:1994-03, table 29, line 2.1.2.1:
  - c<sub>s, req</sub> = 35 mm
  - C<sub>s. exist</sub> = 10 mm
  - $c_{s, req} c_{s, exist} = 35 \text{ mm} 10 \text{ mm} = 25 \text{ mm}$
- Determination of the required application thickness (see diagram 8 on page 14)  $e_{h2}$  = 11 mm

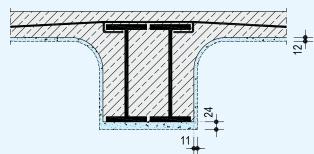
#### Step 4

#### Calculation of the application thickness above the steel beam sections

- A<sub>m</sub>/V value calculation
  - $A_m = b + 2t = 125 \text{ mm} + 2 \cdot 16.2 \text{ mm} = 157.4 \text{ mm} = 15.74 \text{ cm}$
  - $V = b \cdot t = 125 \text{ mm} \cdot 16.2 \text{ mm} = 2025 \text{ mm}^2 = 20.25 \text{ cm}^2$
  - $A_m/V = (15.74 \text{ cm} / 20.25 \text{ cm}^2) \cdot 100 \sim 80 \text{ m}^{-1}$
- Determination of application thickness at REI 90, 500 °C (see table 6 on page 25)  $e_s = 24 \text{ mm}$

#### Step 5

#### Definition of application thickness execution



## **Usage instructions**

## **Notes**



#### Notes on the document

Knauf technical brochures are the information documents on special topics as well as on the specialist competence from Knauf. The contained information and specifications, constructions, details and stated products are based, unless otherwise stated, on the ETA, certificates of usability valid at the time of issue as well as standards and Experts Opinions.

#### References to other documents

#### **Product data sheets**

■ MP 75 Fire P9101\_DSP.de

#### **Technical brochures**

■ Knauf Plaster Competence P10.de

#### **Intended use of Knauf Systems**

Please observe the following:

Caution

Knauf systems may only be used for the application cases specified in the Knauf documentation. In case third-party products or components are used, they must be recommended or approved by Knauf. Flawless application of products / systems assumes proper transport, storage, assembly, installation and maintenance.





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